



RCDC (SACD) V09.02.00

Release Notes

RCDC V09.02.00 is here with new features enhancing the design. The newly introduced features are:

No	Module	Description
1	Column	Gravity Column Design as per IS 13920-2016 & ACI 318
2	Column	Euro Code Column Design Enhancements
3	General	Database Transformation to SQLite
4	General	Enhancements
5	General	Defects - Resolved



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Column

Gravity Column Design as per IS 13920-2016 & ACI 318

RCDC can now support design of Gravity Columns along with Lateral Columns as per 'Ductile Design (Seismic Detailing)' norms and performs the design accordingly. Gravity column design is conforming to following design codes,

- IS 456+13920-2016
- ACI 318M-2011
- ACI 318M-2014
- ACI318-2011
- ACI 318-2014

RCDC can import three different type of Analysis file i.e. STAAD file, RAM SS File and ETABS File. So, following will be the nature of handling columns for each type of analysis file:

- When a STAAD or an ETABS file is imported in RCDC, and user opts to design for Ductility, by Default all the columns will be set to be designed as Lateral Frame Columns.
- When a RAM SS file is imported in RCDC, and user opts to design for Ductility, the frame type of columns (Gravity or Lateral) that will be defined in RAM File will be automatically assigned to each column.

User will be however be allowed to change the Frame type of any column in RCDC itself. For ease of identification, Different types of columns will be represented with different shade of colours in UI.

In case of STAAD and E-Tabs, it may be noted that, effect of 'Gravity Column' intended in analysis must be managed by user with relevant releases etc. In RCDC, the design is handled as per provisions of Gravity Columns for Gravity loads and displacement computability.

An additional input for Response Reduction Factor for Indian code and Response Modification Coefficient for ACI code is required for calculation of additional moment in Gravity column to cater for displacement computability during lateral loads.



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Design Settings

Design Settings

Ductile Setting

Perform Ductile Design

Response Reduction Factor

Live Load Reduction Edit

IS Code

Design Settings

Design Settings

Ductile Setting

Perform Ductile Design

Intermediate Special

Response Modification Coefficient

Live Load Reduction Edit

ACI Code

New tab is added as Frame type in Design Input, where user can define the type of frame,

Design Input								
Column Reference	Column Size	Level Data	Shift Of CG	Frame Type				
LEVEL	C1	C2	C3	C4	C5	C6	C7	C8
4.2m	Non-Ductile	Lateral	Gravity	Non-Ductile	Non-Ductile	Non-Ductile	Non-Ductile	Non-Ductile
7.858m	Non-Ductile	Lateral	Gravity	Non-Ductile	Non-Ductile	Non-Ductile	Non-Ductile	Non-Ductile
12.058m		Lateral	Gravity	Non-Ductile	Non-Ductile	Non-Ductile	Non-Ductile	Non-Ductile
16.258m			Gravity	Non-Ductile	Non-Ductile	Non-Ductile	Non-Ductile	Non-Ductile

In output display, new column is added for Frame type,

Column Design		Design Calculations					
Combined Wall	Column/Wall	Level	Size	Material	Frame Type	Designed As	Capacity Ratio Axial
	C1	0m TO 4.2m	700 X 700	M25 : Fe415	Non-Ductile	COL - E	0.148
	C1	4.2m TO 7.858m	700 X 700	M25 : Fe415	Non-Ductile	COL - E	0.079
	C2	0m TO 4.2m	700 X 700	M25 : Fe415	Lateral	COL - E	0.286
	C2	4.2m TO 7.858m	700 X 700	M25 : Fe415	Lateral	COL - E	0.207
	C2	7.858m TO 12.058m	700 X 700	M25 : Fe415	Lateral	COL - E	0.067
	C3	0m TO 4.2m	700 X 700	M25 : Fe415	Gravity	COL - E	0.45
	C3	4.2m TO 7.858m	700 X 700	M25 : Fe415	Gravity	COL - E	0.379
	C3	7.858m TO 12.058m	700 X 700	M25 : Fe415	Gravity	COL - E	0.253
	C3	12.058m TO 16.258m	700 X 700	M25 : Fe415	Gravity	COL - E	0.118
	C4	0m TO 4.2m	700 X 700	M25 : Fe415	Lateral	COL - E	0.421
	C4	4.2m TO 7.858m	700 X 700	M25 : Fe415	Lateral	COL - E	0.35

Column Reference	Column Size	Level Data	Shift Of CC	Column Layout
LEVEL	C1	C2	C3	
4.2m	Non-Ductile	Lateral	Gravity	
7.858m	Non-Ductile	Lateral	Gravity	
12.058m		Lateral	Gravity	
16.258m			Gravity	

Diagram illustrating the column layout and frame types for columns C1, C2, C3, and C7. The columns are arranged in a grid. C1 and C3 are labeled as Gravity, C2 is labeled as Lateral, and C7 is labeled as Non-Ductile.



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Following are some design Output from RCDC,

Design Summary,

Load Combinations :

- 1 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2)
- 2 1.2 (LOAD 1: LOAD CASE 1) +1.2 (LOAD 2: LOAD CASE 2) +1.2 (LOAD 3: LOAD CASE 3 EQ-X)
- 3 1.2 (LOAD 1: LOAD CASE 1) +1.2 (LOAD 2: LOAD CASE 2) -1.2 (LOAD 3: LOAD CASE 3 EQ-X)
- 4 1.2 (LOAD 1: LOAD CASE 1) +1.2 (LOAD 2: LOAD CASE 2) +1.2 (LOAD 4: LOAD CASE 4 EQ-Y)
- 5 1.2 (LOAD 1: LOAD CASE 1) +1.2 (LOAD 2: LOAD CASE 2) -1.2 (LOAD 4: LOAD CASE 4 EQ-Y)
- 6 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 3: LOAD CASE 3 EQ-X)
- 7 1.5 (LOAD 1: LOAD CASE 1) -1.5 (LOAD 3: LOAD CASE 3 EQ-X)
- 8 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 4: LOAD CASE 4 EQ-Y)
- 9 1.5 (LOAD 1: LOAD CASE 1) -1.5 (LOAD 4: LOAD CASE 4 EQ-Y)
- 10 0.9 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 3: LOAD CASE 3 EQ-X)
- 11 0.9 (LOAD 1: LOAD CASE 1) -1.5 (LOAD 3: LOAD CASE 3 EQ-X)
- 12 0.9 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 4: LOAD CASE 4 EQ-Y)
- 13 0.9 (LOAD 1: LOAD CASE 1) -1.5 (LOAD 4: LOAD CASE 4 EQ-Y)
- 14 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) +3 x Drift- (LOAD 3: LOAD CASE 3 EQ-X)
- 15 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) +3 x Drift- (LOAD 4: LOAD CASE 4 EQ-Y)
- 16 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) -3 x Drift- (LOAD 3: LOAD CASE 3 EQ-X)
- 17 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) -3 x Drift- (LOAD 4: LOAD CASE 4 EQ-Y)

- Levels :
- 1 FOUNDATION
 - 2 4.2m
 - 3 7.858m
 - 4 12.058m
 - 5 16.258m

Column/Wall : C1 FrameType : Non-Ductile

Level	Size (mm)	Material	LC	P (kN)	Mx (kNm)	My (kNm)	Pt (%)	Interaction Ratio	Main Reinforcement	Links
1 TO 2	700 X 700	M25 : Fe415	12	275.04	-28.06	205.81	0.46	0.64	20-T12	T8 @ 175
2 TO 3	700 X 700	M25 : Fe415	7	346.52	338.51	101.27	0.53	0.93	4-T16 + 16-T12	T8 @ 175



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All Load Combination Data

DESIGN DATA FOR ALL LOAD COMBINATIONS

Load Combinations:

- 1 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2)
- 2 1.2 (LOAD 1: LOAD CASE 1) +1.2 (LOAD 2: LOAD CASE 2) +1.2 (LOAD 3: LOAD CASE 3 EQ-X)
- 3 1.2 (LOAD 1: LOAD CASE 1) +1.2 (LOAD 2: LOAD CASE 2) -1.2 (LOAD 3: LOAD CASE 3 EQ-X)
- 4 1.2 (LOAD 1: LOAD CASE 1) +1.2 (LOAD 2: LOAD CASE 2) +1.2 (LOAD 4: LOAD CASE 4 EQ-Y)
- 5 1.2 (LOAD 1: LOAD CASE 1) +1.2 (LOAD 2: LOAD CASE 2) -1.2 (LOAD 4: LOAD CASE 4 EQ-Y)
- 6 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 3: LOAD CASE 3 EQ-X)
- 7 1.5 (LOAD 1: LOAD CASE 1) -1.5 (LOAD 3: LOAD CASE 3 EQ-X)
- 8 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 4: LOAD CASE 4 EQ-Y)
- 9 1.5 (LOAD 1: LOAD CASE 1) -1.5 (LOAD 4: LOAD CASE 4 EQ-Y)
- 10 0.9 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 3: LOAD CASE 3 EQ-X)
- 11 0.9 (LOAD 1: LOAD CASE 1) -1.5 (LOAD 3: LOAD CASE 3 EQ-X)
- 12 0.9 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 4: LOAD CASE 4 EQ-Y)
- 13 0.9 (LOAD 1: LOAD CASE 1) -1.5 (LOAD 4: LOAD CASE 4 EQ-Y)
- 14 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) +3 x Drift- (LOAD 3: LOAD CASE 3 EQ-X)
- 15 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) +3 x Drift- (LOAD 4: LOAD CASE 4 EQ-Y)
- 16 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) -3 x Drift- (LOAD 3: LOAD CASE 3 EQ-X)
- 17 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) -3 x Drift- (LOAD 4: LOAD CASE 4 EQ-Y)

Column/Wall : C3
 Level : 0m To 4.2m
 Frame Type : Gravity
 Design Code = IS 456 + IS 13920 - 2016
 Grade of Concrete = 25 N/sqmm
 Grade of Steel = 415 N/sqmm
 Column B = 700 mm
 Column D = 700 mm
 Clear Cover = 50 mm
 Pt = 0.82 %

Design Table :

Member	LOC	I/C	Pu (kN)	Analysis		Min ECC		Slenderness		Design			MCap (kNm)	Capacity Ratio
				Mx (kNm)	My (kNm)	Mx (kNm)	My (kNm)	Mx (kNm)	My (kNm)	Mux (kNm)	Muy (kNm)	MuRes (kNm)		
201	BOT	1(a)	2476.25	6.24	-17.21	74.62	-	0	0	74.62	-17.21	76.58	717.24	0.11
201		1(b)	2476.25	6.24	-17.21	-	74.62	0	0	6.24	-74.62	74.88	737.94	0.1
201	TOP	8(a)	1788.48	6.34	-77.43	53.89	-	0	0	53.89	-77.43	94.34	647.72	0.15
201		8(b)	1788.48	6.34	-77.43	-	53.89	0	0	6.34	-77.43	77.69	719.03	0.11
201	BOT	9(a)	2393.85	17.89	-233.57	72.13	-	0	0	72.13	-233.57	244.45	705.28	0.35
201		9(b)	2393.85	17.89	-233.57	-	72.13	0	0	17.89	-233.57	234.25	739.16	0.32
201	TOP	9(a)	2316.65	-7.52	112.14	69.81	-	0	0	-69.81	112.14	132.09	664.02	0.2
201		9(b)	2316.65	-7.52	112.14	-	69.81	0	0	-7.52	112.14	112.39	740.58	0.15
201	BOT	13(a)	1541.95	15.76	-228.38	46.46	-	0	0	46.46	-228.38	233.06	686.78	0.34
201		13(b)	1541.95	15.76	-228.38	-	46.46	0	0	15.76	-228.38	228.93	700.78	0.33
201	TOP	13(a)	1495.62	-7.29	105.2	45.07	-	0	0	-45.07	105.2	114.45	655.08	0.17
201		13(b)	1495.62	-7.29	105.2	-	45.07	0	0	-7.29	105.2	105.45	696.44	0.15

Gravity Load Combination :

Member	LOC	I/C	Pu (kN)	Analysis		Storey Drift		Additional Moment		Design			Mcap (kNm)	Capacity Ratio
				Mx (kNm)	My (kNm)	Δx (mm)	Δy (mm)	Mx (kNm)	My (kNm)	Mux (kNm)	Muy (kNm)	MuRes (kNm)		
201	BOT	14(a)	2476.25	6.24	-17.21	1.14	0.02	8.49	0.18	14.73	-17.03	22.52	649.01	0.03
201	TOP	14(a)	2399.04	-0.66	21.74	1.14	0.02	8.23	0.18	7.57	21.92	23.19	699.66	0.03
201	BOT	15(a)	2476.25	6.24	-17.21	0	0.95	0.03	7.05	6.28	-10.17	11.95	663.67	0.02
201	TOP	15(a)	2399.04	-0.66	21.74	0	0.95	0.03	6.83	-0.63	28.57	28.58	745.59	0.04
201	BOT	16(a)	2476.25	6.24	-17.21	1.14	0.02	-8.49	-0.18	-2.25	-17.4	17.54	731.88	0.02
201	TOP	16(a)	2399.04	-0.66	21.74	1.14	0.02	-8.23	-0.18	-8.89	21.56	23.32	689.48	0.03
201	BOT	17(a)	2476.25	6.24	-17.21	0	0.95	-0.03	-7.05	6.21	-24.26	25.04	713.16	0.04
201	TOP	17(a)	2399.04	-0.66	21.74	0	0.95	-0.03	-6.83	-0.7	14.91	14.93	742.78	0.02



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Design Calculation, Flexural Check

Flexure Design (Displacement Compatibility)

Load Combination	=	[15] : 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) +3 x Drift- (LOAD 4: LOAD CASE 4 EQ-Y)
Critical Location	=	Top Joint
Pu	=	2399.04 kN
Mx	=	-0.66 kNm
My	=	21.74 kNm
Drift Along X (Δ_x)	=	0 mm
Drift Along Y (Δ_y)	=	0.95 mm
Additional Moment along X ($M_{ux \text{ add}}$)	=	0.03 kNm
Additional Moment along Y ($M_{uy \text{ add}}$)	=	6.83 kNm
Mux	=	-0.63 kNm
Muy	=	28.57 kNm

Resultant Moment (Combined Action)

Moment Capacity Check

Pt Calculated	=	0.46
Reinforcement Provided	=	20-T12

Load Angle	=	$\tan^{-1}(M_{uy}/M_{ux})$
	=	88.74 deg
MRes	=	28.58 kNm
MCap	=	621.44 kNm
Capacity Ratio	=	MRes/ MCap
	=	0.05 <= 1

Design Calculation, Shear Check

Shear Design (Displacement Compatibility)

Design for shear along D

Critical Load Combination	=	[15] : 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) +3 x Drift- (LOAD 4: LOAD CASE 4 EQ-Y)
Design shear force, Vuy	=	1.6442 kN
Pu	=	2476.25 kN
Drift Along X (Δ_x)	=	0 mm
Drift Along Y (Δ_y)	=	0.95 mm
Additional Moment along Y ($M_{uy \text{ add}}$)	=	7.05 kNm
Additional Shear Y	=	1.68 kN
Total Shear, Vuy	=	3.32 kN
Deff	=	644 mm
Design shear stress, Tvy	=	$V_{uy} / (B_x \text{ Deff})$ N/sqmm
	=	0.0074 N/sqmm
Pt	=	0.231 %
Design shear strength, Tc	=	0.3523 N/sqmm
Shear Strength Enhancement Factor	=	$1 + 3 \times P_u / (B \times D \times F_{ck})$
	=	1.6064
Shear Strength Enhancement Factor (max)	=	1.5
Shear Strength Enhancement Factor	=	1.5
Enhanced shear strength, Tc-e	=	0.5284 N/sqmm
Design shear check	=	$T_{vy} < T_c \times \text{Enhancement factor}$

Link for Shear Design along D are not required



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Design of Links as per stress level for Gravity Load combinations.

Design Of Links

Links in the zone where special confining links are not required

Normal Links

Diameter of link	=	8	mm
	>	Max. longitudinal bar dia / 4	
	=	4	mm

Criterion for spacing of normal links

Min. Longitudinal Bar dia X 16	=	256	mm
Min. dimension of column	=	700	mm
Max. 300 mm	=	300	mm
Least lateral edge dimension/2	=	350	

Check for Links

Critical Load Combination	=	[14] : 1.5 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) +3
Pu	=	2476.25 kN
Actual Axial Stress	=	Pu / (B x D)
	=	5.05 N/sqmm
Threshold Axial Stress	=	0.4 x fck
	=	10 N/sqmm
	=	5.05 < 10 Non Ductile links are applicable

Criterion for spacing

6 x Smallest Longitudinal Bar Dia	=	96	mm
Maximum Spacing	=	150	mm
Provided spacing	=	75	mm

Links to be Provided along full height of Column

Column Euro Code Column Design Enhancements

Column design as per Euro Code has been updated with some additional inputs from users. In the earlier version's effective length factor and some constant required for slenderness check had been assumed. Now the values for ϕ_{ef} and the input for 'Type of frame' could be modified by user in RCDC.

The screenshot shows the 'Design Settings' dialog box with several options checked: 'Perform Ductile Design', 'Effective Length Factor', and 'Type of Frame' set to 'UnBraced'. A separate window titled 'Effective Creep Ratio (ϕ_{ef})' is open, displaying a table with 'Edge Length' and ' ϕ_{ef} ' values.

Edge Length	ϕ_{ef}
300	2.142
350	2.142
500	2.142
600	2.142
700	2.142
900	2.142
2400	2.142
3550	2.142

Presentation of calculations in the report is improved. Sample design calculation report is as below,



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Calculation of SLENDERNESS CHECK

	Along D	Along B
Critical Load Combination	[5] : 1.35 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) -(LOAD 4: LOAD CASE 4 EQ-Y)	[5] : 1.35 (LOAD 1: LOAD CASE 1) +1.5 (LOAD 2: LOAD CASE 2) -(LOAD 4: LOAD CASE 4 EQ-Y)
Ned (kN)	2439.33	2439.33
Mo1 (kNm)	5.23	83.2
Mo2 (kNm)	14.07	162.99
Radius of Gyration (i) (mm)	173.41	173.41
Φ_{ef}	2.14	2.14
$A = 1 / (1 + 0.2 \times \Phi_{ef})$	0.7	0.7
$B = \text{Sqrt} (1 + 2 \omega)$	1.12	1.12
$rm = Mo1 / Mo2$	-0.37	-0.51
$C = 1.7 - rm$	2.07	2.21
$n = Ned / (B \times D \times f_{cd})$	0.4066	0.4066
Slenderness ratio (λ) = l_0 / i	52.76	52.76
Permissible Limits (λ_{lim}) = $A \times B \times C / \text{sqrt} (n)$	50.9	54.35
	Hence, Column is Slender	Hence, Column is not Slender

Calculation of Slenderness Moment

	Along D	Along B
$\eta u = 1 + \omega$	1.13	---
nbal	0.4	---
$K_r = \text{Min} ((\eta u - n) / (\eta u - n_{bal}), 1)$	0.99	---
c (Constant)	10	---
Is (mm)	173.41	---
deff, slenderness = $(D' / 2) + Is$ (mm)	274.58	---
$\beta = 0.35 + f_{ck} / 200 - \lambda / 150$	0.098	---
$1 / r_0 = f_{yd} / E_s \times (0.45 \times \text{deff, slenderness}) \times 10^{-5}$	1.7	---
$K \phi = \text{Max} ((1 + \beta \times \Phi_{ef}), 1)$	1.21	---
$1 / r = K_r \times K \phi \times (1 / r_0) \times 10^{-5}$	2.04	---
$e_2 = (1 / r) \times (l_0^2 / c)$ (mm)	170.68	---
$M_{oe} = 0.4 \times \text{Min} (\text{top, bottom}) + 0.6 \times \text{Max} (\text{top, bottom})$ (kNm)	64.37	---
$M_2 = e_2 \times Ned$ (kNm)	416.34	---
Mid Moment = $M_{oe} + M_2$ (kNm)	480.71	---

General Database Transformation to SQLite

RCDC used PostgreSQL as Database to save the entire Project Data / information.

We have now enhanced the Database type from Postgres to SQLite.

This would help stabilize the installation related issues and eliminate need of external database.

The internal Design and Detail Functionalities remain same as the earlier versions of RCDC. This transformation has NO Impact on any Design or Detail for any Module in RCDC other than enhancements in this release.



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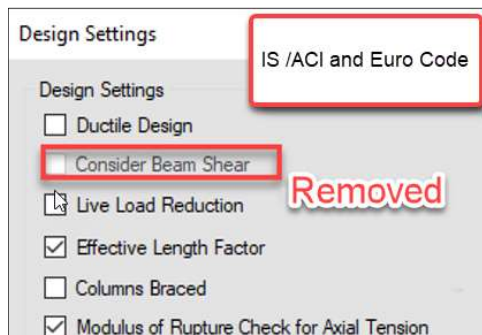
General Enhancements

Following are the Enhancements are done in this release.

- TFS ID – 1050918**

Consider beam shear option for ductile design is now mandatory in IS, ACI and Euro codes.

The option of Beam shear is now removed from design settings of column design. As per codes, it is part of Ductile design, thus now onwards the check related to beam shear will be performed in RCDC.



- TFS ID – 1063418**

ϕV_c in ACI Beam design for special frame type has been considered as Zero. The capacity of the concrete in case of Special frame has been ignored.

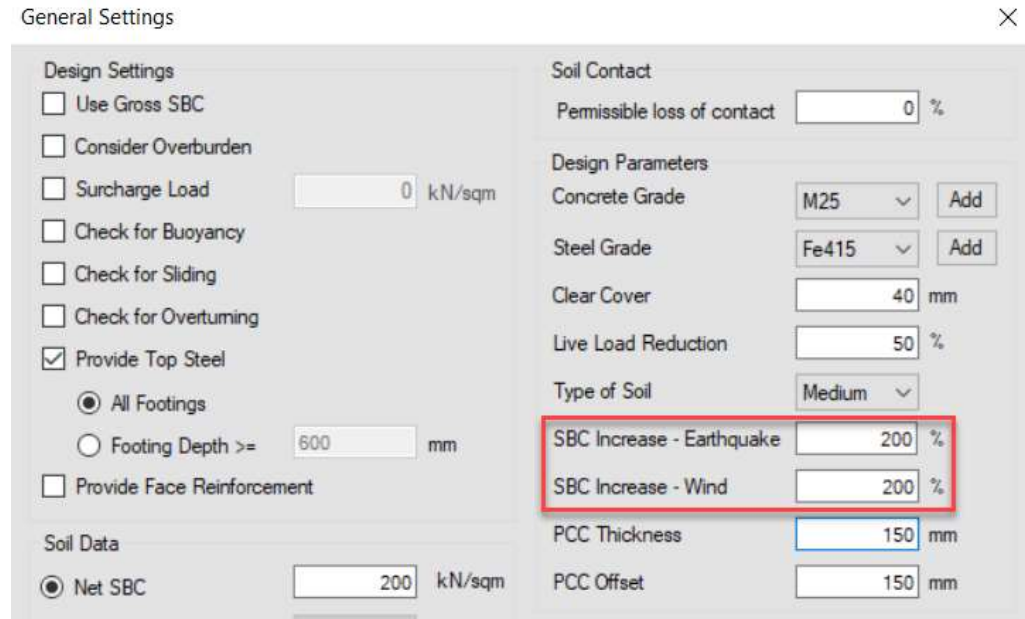
For Transverse Reinf	Left	Mid	Right
Critical L/C - RCDC	5	4	4
PtPrv (%)	0.694	0.174	0.694
Vu (kN)	215.69	156.22	235.41
Mu-Sect (kNm)	355.79	30.03	432.53
V ^{D+L} (kN)	163.47	0	161.83
Mh (kNm)	693.53	0	693.53
Ms (kNm)	234.62	0	367.59
Sway-Right (kN)	36.32	0	288.98
Sway-Left (kN)	308.82	0	16.48
Vu-Sway (kN)	308.82	0	288.98
Vud (kN)	308.82	0	288.98
ϕV_c (kN)	0	0	0
Vs (kN)	359.48	260.37	392.35
Av (sqmm/m)	1172.46	849.2	1279.68
Tu (kNm)	1.41	1.46	1.46
Aoh (sqmm)	-	-	-
At (sqmm/m)	-	-	-
Legs	2	2	2
Stirrup Rebar	10	10	10
At Torsion (sqmm/m)	0	0	0
Av Total Reqd (sqmm/m)	1172.46	849.2	1279.68
Asv Reqd (sqmm/m)	1678.76	849.2	1570.87
S _{Calc} (mm)	75	165	75
S _{Prv} (mm)	75	165	75
Av Total Prv (sqmm/m)	1890.13	859.15	1890.13



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- **TFS ID – 1077894**

Option of Providing SBC increased up to 200% for Earthquake and Wind load combinations. This is applicable to all design codes and applicable for Footing and pile-cap design.



This has been added to cater for specific cases reported by user, where permissible SBC for gravity loads is very low compared to the same for Load combinations with lateral loads.

General Defects

- **TFS ID – 1069329**

Joint check In Column design - Beam orientation with respect to column major axis was not considered correctly in a few cases.

Issue has been resolved and correct orientation is considered in design for all possible conditions.

Check At Beam-Column Joints:

1. Flexure Strength Of Joint:

Moment Capacity Calculations for Beam

Beam Size (mm)	Beam angle w.r.t. column Ly (deg)	Torsion moment (kNm)	Moment Capacity Beam at Top				Moment Capacity Beam at Bottom				Resultant Moment			
			Mu (kNm)	Ast Req (sqmm)	Ast Pro (sqmm)	Mu Cap (kNm)	Mu (kNm)	Ast Req (sqmm)	Ast Pro (sqmm)	Mu Cap (kNm)	Top @ D (kNm)	Top @ B (kNm)	Bot @ D (kNm)	Bot @ B (kNm)
400 x 700	0	0	313.47	1489.55	1570.8	328.64	62.44	746.02	804.24	177.55	328.64	0	177.55	0
400 x 700	90	0	310.21	1472.23	1570.8	328.64	177.54	804.19	804.24	177.55	0	328.64	0	177.55
400 x 700	180	0	313.47	1489.55	1570.8	328.64	62.44	746.02	804.24	177.55	328.64	0	177.55	0
400 x 700	270	0	310.21	1472.23	1570.8	328.64	177.54	804.19	804.24	177.55	0	328.64	0	177.55



RCDC (SACD) V09.02.00

- TFS ID – 1069337**

Joint check In Column design - beam top end moment was incorrectly considered only if beam consists of more than one member in STAAD.

Now the correct top moment is considered in the calculation of Ast required and Beam capacity is calculated accordingly.

Check At Beam-Column Joints:

1. Flexure Strength Of Joint:

Moment Capacity Calculations for Beam

Beam Size	Beam angle w.r.t. column Ly	Torsion moment	Moment Capacity Beam at Top				Moment Capacity Beam at Bottom				Resultant Moment			
			Mu (kNm)	Ast Req (sqmm)	Ast Pro (sqmm)	Mu Cap (kNm)	Mu (kNm)	Ast Req (sqmm)	Ast Pro (sqmm)	Mu Cap (kNm)	Top @ D (kNm)	Top @ B (kNm)	Bot @ D (kNm)	Bot @ B (kNm)
400 x 700	0	0	313.47	1489.55	1570.8	328.64	62.44	746.02	804.24	177.55	328.64	0	177.55	0
400 x 700	270	0	310.21	1472.23	1570.8	328.64	177.54	804.19	804.24	177.55	0	328.64	0	177.55

- TFS ID – 1070763**

ACI code Column Design - Effective length calculation in column design was not supported if only wind load cases are considered in the design. (No Earthquake loads)

Issue has been resolved.

Sway Calculation (Stability Index)

For Global-X Direction

Level	Load Combination	Story Height (m)	Gravity Load P (kN)	Relative Displacements (mm)	Story Shear (kN)	Stability Index (Q)	Sway Condition
		A	B	C	D	B x C / (A x D)	
0m to 4.2m	8	4.2	65936	1.84	2807.52	0.01	Non Sway
4.2m to 7.858m	9	3.66	57493.68	2.22	2705.08	0.013	Non Sway
7.858m to 12.058m	9	4.2	34863.97	2.7	2320.93	0.01	Non Sway
12.058m to 16.258m	8	4.2	14317.6	1.99	1624.65	0.004	Non Sway

- TFS ID – 1077204**

Software was crashing if design was performed using ACI English unit design codes if there was Shear wall with parametric surface in the (STAAD Analysis) file.

Issue has been resolved related to parametric surface for English unit ACI design codes.