

TITLE :	DESIGN OF BEAM																
SUB -TITLE :	DESIGN OF BEAM FOR FLEXURE,SHEAR AND TORSION																
CODE OF PRACTICE :	IS 456 : 2002																
CODE TITLE :	PLANE AND REINFORCED CONCRETE																
DESIGN TYPE :	LIMIT STATE DESIGN																
NOTE :- 1) User to Input data in cell marked as Blue.																	
2) Design follows Limit State Method.																	
3) Forces of one section has been considered for design																	
Step 1) User Input																	
PARAMETERS :					SYMBOL		USER INPUT		UNITS		Reference / Comments						
Beam No							B6				User Input						
Reference section of Beam							Top Left				User Input						
Width of Beam					B		400	mm			User Input						
Depth of Beam					D		900	mm			User Input						
Thickness of Slab					Df		0	mm									
Type of beam							Rectangular				User Input						
Bending Moment from Analysis at section considered					Mu		1,026.51	kN-m			User Input						
Shear force from analysis at section considered					Vu		628.28	kN			User Input						
Torsion force from analysis at section considered					Tu		61.05	kN-m			User Input						
characteristic compressive strength of concrete (Cube Strength)					fck		25.00	N/mm <sup>2</sup>			User Input						
characteristic strength of reinforcement					fy		415.00	N/mm <sup>2</sup>			User Input						
Cover to tension reinforcement					Cc		25.00	mm			User Input						
Cover to compression reinforcement					Cc'		25.00	mm			User Input						
Diameter of tenson reinforcement					dia1		20.00	mm			User Input						
Diameter of comression reinforcement					dia2		20.00	mm			User Input						
Diameter of shear reinforcement					dia3		10.00	mm			User Input						
Diameter of SFR					dia4		12.00	mm			User Input						
Number of legs for shear reinforcement							2	nos			User Input						
Number of reinforcement layers at tension face					n1		2.00	Nos			User Input						
Number of reinforcement layers at compression face					n2		2.00	Nos			User Input						
Depth of flange							100	mm			User Input						
Partial Factor of Safety for Material Concrete					γm concrete		1.50	constant			Clause 36.4.2.1						
Partial Factor of Safety for Material Steel					γm steel		1.15	constant			Clause 36.4.2.1						
Detailing of Tension reinforcement																	
Number of reinforcement at first layer							4	nos			User Input						
Number of reinforcement at second layer							3	nos			User Input						
Reinforcement diameter at first layer							32	mm			User Input						
Reinforcement diameter at second layer							25	mm			User Input						
Detailing of Compression reinforcement																	
Number of reinforcement at first layer							4	nos			User Input						
Number of reinforcement at second layer							0	nos			User Input						
Reinforcement diameter at first layer							20	mm			User Input						
Reinforcement diameter at second layer							16	mm			User Input						
characterstic yield strength of einforcement for shear					fyt		415.00	N/mm <sup>2</sup>			Clause 26.5.1.6						
Effective depth at tension face					deff		845.00	mm			User Input						
Effective cover at compression reinforcement					d'		55.00	mm									

$f_y$  = characteristic strength of the stirrup reinforcement in N/mm<sup>2</sup> which shall not be taken greater than 415 N/mm<sup>2</sup>.

Step 2) Design for singly reinforced section									
Equivalent Bending moment due to torsion				Mt		116.71		kN-m	Clause 41.4.2
Equivalent Moment due to torsion				Me1		1143.22		kN-m	Clause 41.4.2
Balance neutral axis				Xu bal		(0.0035/(0.0055+(0.87*fy/(2*10^5))))*deff			Clause 38.1
						404.85		mm	
limiting moment of resistance of a section without compression reinforcement,				Mu lim		0.36*fck*Xu bal*B*(deff-0.416*Xu bal)/10^6			
						986		kN-m	Clause 38.1
Mu/bd^2				R		4.003			
Check						Doubly reinforced.refer step-3			
Minimum % reinforcement				Ptmin		0.205		%	Clause 26.5.1.1
Ast minimum				Astmin		692.29		sqmm	Clause 26.5.1.1
Area of tension reinforcement required				Ast req		-		sqmm	Annex -G (G.1)
% tension steel required				ptcalc		-		%	
Area of compression reinforcement for torsion				Asc req		-		sqmm	Clause 41.4.2.1
Step 3) Design of doubly reinforced section									
Determining area of compression reinforcement									
Strain at level of compression reinforcement				Esc		=0.0035*(1-(d'/Xu bal))			
						0.003025			
stress in compression reinforcement				fsc		354.14		N/sqmm	Annex -G (G.1)
Area of compression reinforcement				Asc req		561.67		sqmm	Annex -G (G.1)
% compression steel required						(Asc req*100/(B*deff))*0.87*fy/(fsc-0.446*fck)			
						0.175		%	
Ast of tension reinf. required for balance section				Ast1		4036.68		sqmm	Annex -G (G.1)
Area of tension reinforcement required for doubly section				Ast2		550.92		sqmm	Annex -G (G.1)
Total Area of tension reinforcement				Ast req		4,587.6		sqmm	Annex -G (G.1)
% tension steel required				ptcalc		1.357		%	
Area of tension reinforcement provided				Ast provided		4690		sqmm	
Check for tension reinforcement						OK			
Area of compression reinforcement provided				Asc provided		1257		sqmm	
Check for compression reinforcement						OK			

$$M_{u,lim} = 0.36 \frac{x_{u, max}}{d} \left( 1 - 0.42 \frac{x_{u, max}}{d} \right) b d^2 f_{ck}$$

The longitudinal reinforcement shall be designed to resist an equivalent bending moment,  $M_{e1}$ , given by

$$M_{e1} = M_u + M_t$$

where

$$M_u = \text{bending moment at the cross-section, and}$$

$$M_t = T_u \left( \frac{1+D/b}{1.7} \right)$$

$$M_u - M_{u,lim} = f_{sc} A_{sc} (d - d')$$

where

$$M_u, M_{u, lim}, d \text{ are same as in G-1.1,}$$

$$f_{sc} = \text{design stress in compression reinforcement corresponding to a strain of}$$

$$0.0035 \frac{(x_{u, max} - d')}{x_{u, max}}$$

The total area of tension reinforcement shall be obtained from the following equation :

$$A_{st} = A_{st1} + A_{st2}$$

where

$$A_{st} = \text{area of the total tensile reinforcement,}$$

$$A_{st1} = \text{area of the tensile reinforcement for a singly reinforced section for } M_{u, lim}, \text{ and}$$

$$A_{st2} = A_{sc} f_{sc} / 0.87 f_y.$$

<b>Step 4) Design of Shear reinforcement</b>									
shear due to torsion		Vtu	244.20	kN	Clause B-6.3				
Total shear		Vut	872.48	kN	Clause B-6.3				
Nominal shear stress		Tv	2.58	N/sqmm	Clause 40.1 and 41.3.1				
Maximum shear stress		Tcmax	3.1	N/sqmm	Table 20				
Check			OK						
Design strength of concrete		Tc	0.72	N/sqmm	Table 19				
Shear Capacity of Concrete		Vc	244.15	kN	Table 19				
Shear to be carries by Reinforcement		Vus=Vut-Vc	628.33	kN	Clause 40.4 (a)				
Total shear reinforcement required		Asv req	2059.50	sqmm/m	Clause 40.4 (a)				
C/C distance between corner bars in direction of width		b1	318.00	mm					
C/C distance between corner bars in direction of depth		d1	818.00	mm					
shear reinforcement to be provided at outer link		Asv torsion	1500.96	sqmm/m	Clause 41.4.3				
Area of Shear reinforcement provided		Asv Total Prv	2094.40	sqmm/m					
<b>Stirrups Spacing Criteria</b>									
Short dimension of stirrups		x1	360	mm	Clause 26.5.1.7				
long dimension of stirrups		y1	860	mm	Clause 26.5.1.7				
		spc1	634	mm	Clause 26.5.1.5				
		Spc2	300	mm	Clause 26.5.1.5				
		Spc3	360	mm	Clause 26.5.1.7				
		Spc4	305	mm	Clause 26.5.1.7				
Spacing of links		SvCalc	75	mm					
Spacing required for outer stirrups			105	mm					
Spacing to be provided		SvPrv	75	mm					
<b>Step 5) Side face reinforcement</b>									
Width of Beam		B	400	mm					
Depth of Beam (Web Depth) D- Df		D	900	mm					
Torsion			61.05>0	kN-m	Clause 26.5.1.7				
			900>750		Clause 26.5.1.3				
Check			SFR required		Clause 26.5.1.3				
Total side face reinforcement required		ASFR	360	Sqmm	Clause 26.5.1.3				
Numbers of reinf required			2						
Area of SFR provided		ASFR Provided	452.39	Sqmm					
Check for spacing			OK		Clause 26.5.1.3				
<b>Spacing Criteria</b>									
Provided Spacing			231.33	mm					
		<= beam Width	400	mm	Clause 26.5.1.7				
		Not Greater Than	300	mm	Clause 26.5.1.7				

#### B-6.4.3 Transverse Reinforcement

Two legged closed hoops enclosing the corner longitudinal bars shall have an area of cross-section  $A_{sv}$ , given by

$$A_{sv} = \frac{T.s_v}{b_1 d_1 \sigma_{sv}} + \frac{V.s_v}{2.5 d_1 \sigma_{sv}}, \text{ but the total}$$

transverse reinforcement shall not be less than

$$\frac{(\tau_{ve} - \tau_c) b.s_v}{\sigma_{sv}}$$

#### 26.5.1.7 Distribution of torsion reinforcement

When a member is designed for torsion (see 41 or B-6) torsion reinforcement shall be provided as below:

- The transverse reinforcement for torsion shall be rectangular closed stirrups placed perpendicular to the axis of the member. The spacing of the stirrups shall not exceed the least of  $x_1$ ,  $\frac{x_1 + y_1}{4}$  and 300 mm, where  $x_1$  and  $y_1$  are respectively the short and long dimensions of the stirrup.
- Longitudinal reinforcement shall be placed as close as is practicable to the corners of the cross-section and in all cases, there shall be at least one longitudinal bar in each corner of the ties. When the cross-sectional dimension of the member exceeds 450 mm, additional longitudinal bars shall be provided to satisfy the requirements of minimum reinforcement and spacing given in 26.5.1.3.

#### 26.5.1.3 Side face reinforcement

Where the depth of the web in a beam exceeds 750 mm, side face reinforcement shall be provided along the two faces. The total area of such reinforcement shall be not less than 0.1 percent of the web area and shall be distributed equally on two faces at a spacing not exceeding 300 mm or web thickness whichever is less.