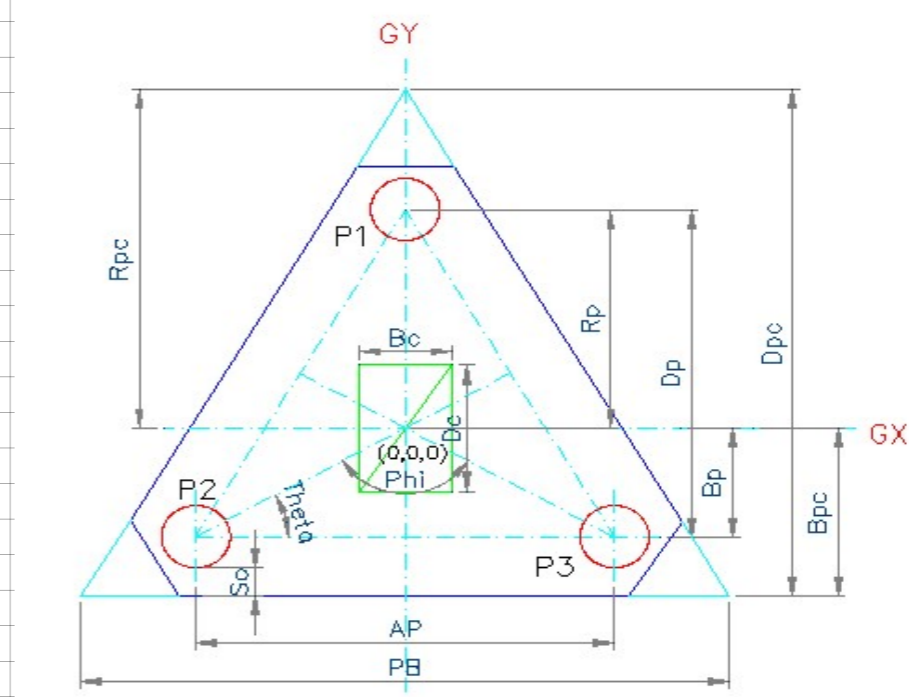


Forces from Service load Combinations (maximum Shear on one Pile)					
Governing Load combination				Lateral	User Input
Shear along Major Direction		Vx	2.61	kN	User Input
Shear along Minor Direction		Vy	65.45	kN	User Input
Forces from Service load Combinations (Uplift on one pile)					
Governing Load combination				Lateral	User Input
Self Weight multiplying factor for load check (Uplift load on pile)			1.00		User Input
Axial Force		Pcomb	-	kN	User Input
Moment along Major Direction		Mx	-	kN-m	User Input
Moment along Minor Direction		My	-	kN-m	User Input
Forces from Limit load Combinations (Bottom reinforcement Along parallel Edge)					
Self Weight multiplying factor for load check (Bottom reinf. Along Parallel Edge)			1.20		User Input
Axial Force		Pu	4,054.19	kN	User Input
Moment along Major Direction		Mux	-23.23	kN-m	User Input
Moment along Minor Direction		Muy	-8.19	kN-m	User Input
Forces from Limit load Combinations (Bottom reinforcement Along Perpendicular Edge)					
Self Weight multiplying factor for load check (Bottom reinf. Along perpendicular Edge)			1.20		User Input
Axial Force		Pu	3,609.75	kN	User Input
Moment along Major Direction		Mux	-341.99	kN-m	User Input
Moment along Minor Direction		Muy	-9.12	kN-m	User Input
Forces from Limit load Combinations (One way shear-Along Parallel Edge)					
Self Weight multiplying factor for load check (One way shear. Along parallel Edge)			1.20		User Input
Axial Force		Pu	4,054.19	kN	User Input
Moment along Major Direction		Mux	-23.23	kN-m	User Input
Moment along Minor Direction		Muy	-8.19	kN-m	User Input
Forces from Limit load Combinations (One way shear-Along Perpendicular Edge)					
Self Weight multiplying factor for load check (Onnway shaer. Along perpendicular Edge)			1.20		User Input
Axial Force		Pu	3,609.75	kN	User Input
Moment along Major Direction		Mux	-341.99	kN-m	User Input
Moment along Minor Direction		Muy	-9.12	kN-m	User Input
Forces from Limit load Combinations (Load Transfer Check)					
Axial Force		Pu	4,054.19	kN	User Input
Detailing of Bottom/Top reinforcement					
Spacing of reinforcement at Bottom Along parallel edge			130		User Input
Reinforcement diameter at Bottom along parallel edge			25.40	mm	User Input
Number of reinforcement at Bottom Along perpendicular edge			115		User Input
Reinforcement diameter at Bottom along perpendicular edge			25.40	mm	User Input
Number of reinforcement at Top Along parallel edge			145		User Input
Reinforcement diameter at Top Along parallel edge			15.90	mm	User Input
Number of reinforcement at Top Along perpendicular edge			145	nos	User Input
Reinforcement diameter at Top Along perpendicular edge			15.90	mm	User Input
Shear Reinforcement					
Along Parallel edge					
Diameter of shear reinf.		dia3	15.90	mm	User Input
Legs			5	mm	User Input
Spacing			100	mm	User Input
Along Perpendicular edge					
Diameter of shear reinf.		dia3	15.90	mm	User Input
Legs			8	mm	User Input
Spacing			105	mm	User Input
SFR provided					
Diameter of SFR		dia4	9.50	mm	User Input
Number of SFR			3	nos	User Input

11.4.2 — The values of f_y and f_{yt} used in design of shear reinforcement shall not exceed 420 MPa



SKETCH-01

characteristic yield strength of reinforcement for shear			fyt	420.00	N/mm ²	clause 11.4.2												
Step 2) Pile and Pile group capacities																		
Pile Capacity			Ppile axial	1,375	kN													
Pile Group Capacity			Pgroup	4125	kN													
Pile Group Capacity in shear			Ppile shear	200	kN													
Pile capacity in tension			Ppile tension	150	kN													
Step 3) Pilecap configuration and geometry (refer sketch-01)																		
C/C distance Between pile		D x factor	Ap	1875	mm													
		$360/(\text{No of Piles}) \cdot \pi / 180$	Phi	2.094	Radian													
		$(180 - (360/(\text{No of Piles}))) / 2 \cdot \pi / 180$	Theta	0.524	Radian													
		$Ap/2 \cdot \tan(\text{Theta})$	Bp	541.27	mm													
Pile-cap Base		$(Bp + \text{Offset} + (D/2)) / Bp \cdot Ap$	PB	3,693.65	mm													
		$\text{SQRT}((Ap/2)^2 + Bp^2)$	Rp	1082.53	mm													
		$Ap/2 \cdot \tan(2 \cdot \text{Theta})$	Dp	1,623.80	mm													
		$\text{Offset} + Bp + D/2$	Bpc	1,066.27	mm													
		$\text{SQRT}((PB/2)^2 + Bpc^2)$	Rpc	2132.53	mm													
		$PB \cdot \sin(\text{Phi})$	Dpc	3198.80	mm													
		Area of pilecap		5430228	sqmm													
<table border="1"> <thead> <tr> <th>Position of Piles</th> <th>Px</th> <th>Py</th> </tr> </thead> <tbody> <tr> <td>P1</td> <td>0</td> <td>1083</td> </tr> <tr> <td>P2</td> <td>937.5</td> <td>541</td> </tr> <tr> <td>P3</td> <td>937.5</td> <td>541</td> </tr> </tbody> </table>							Position of Piles	Px	Py	P1	0	1083	P2	937.5	541	P3	937.5	541
Position of Piles	Px	Py																
P1	0	1083																
P2	937.5	541																
P3	937.5	541																
Step 4) Check for maximum load on one pile																		
Forces On Piles																		
Weight of pilecap + Overburden weight of soil		Soil Wt. + Pile-cap Wt.		391.405	kN													
Total Weight on Pile		Pcomb + Soil Wt. + Pile-cap Wt.	Ptotal	3,355.79	kN													
Load transfer to pile P1		$P_{total}/(\text{No of Piles}) - (M_x/(D_p/1000))$		1,202.71	kN													
Load transfer to pile P2		$P_{total}/(\text{No of piles}) + (M_x/(D_p \cdot 2/1000)) - (M_y/(A_p/1000))$		1079.97	kN													
Load transfer to pile P3		$P_{total}/(\text{No of piles}) + (M_x/(D_p \cdot 2/1000)) + (M_y/(A_p/1000))$		1073.10	kN													
Ptotal																		
Maximum load on one pile		Max(P1,P2,P3)		1,202.71	kN													
Allowable load on pile			Ppile axial	1,375	kN													
Check				OK														
Step 5) Check for maximum load on pile group																		
Weight of pilecap + Overburden weight of soil		Soil Wt. + Pile-cap Wt.		391.405	kN													
Total Weight on Pile		Pcomb + Soil Wt. + Pile-cap Wt.		3,539.71	kN													
Maximum load on pile group				3,539.71	kN													
Allowabl load on pile group			Pgroup	4,125	kN													
Check				OK														
Step 6) Check for maximum shear on pile group																		
Maximum shear on pile group		$\text{SQRT}(V_x^2 + V_y^2)$		65.50	kN													
Shear Capacity of pile group		Shear capacity x no of Pies	Ppile shear	600	kN													
Check																		
Step 7) Check for uplift on one pile																		
Weight of pilecap + Overburden weight of soil		Soil Wt. + Pile-cap Wt.		-	kN													
Total Weight on Pile		Pcomb + Soil Wt. + Pile-cap Wt.	Ptotal	-	kN													
Load transfer to pile P1		$P_{total}/(\text{No of Piles}) - (M_x/(D_p/1000))$		-	kN													
Load transfer to pile P2		$P_{total}/(\text{No of piles}) + (M_x/(D_p \cdot 2/1000)) - (M_y/(A_p/1000))$		0.00	kN													
Load transfer to pile P3		$P_{total}/(\text{No of piles}) + (M_x/(D_p \cdot 2/1000)) + (M_y/(A_p/1000))$		0.00	kN													

Maximum tensile load on pile group				-	kN	
Allowabl load on pile group			Ppile tension	150	kN	
Check				OK		
Step 8)Design for Bending						
Weight of pilecap + Overburden weight of soil		Soil Wt. + Pile-cap Wt.		469.69	kN	
Total Weight on Pile		Pcomb + Soil Wt. + Pile-cap Wt.	Ptotal	4,523.88	kN	
Forces On Piles						
Load transfer to pile P1		Ptotal/(No of Piles)-(Mux/(Dp/1000))		1,522.26	kN	
Load transfer to pile P2		Ptotal/(No of piles)+(Mux/(Dp*2/1000))-(Muy/(Ap/1000))		1,505.17	kN	
Load transfer to pile P3		Ptotal/(No of piles)+(Mux/(Dp*2/1000))+(Muy/(Ap/1000))		1,496.44	kN	
Bottom reinforcement Along Parallel Edge						
Effective depth of pilecap		Depth - cover - 20- 20/2	Deff	670.00	mm	
Effective width of pile cap		Pile dia + 2 x Offset	Beff	1,050	mm	
offset from column face		(Ap/2-Bc/2)/1000	DfCol	0.64	m	
Bending moment due to pile load			Bmux	959.55	kN-m	
% reinf. Required for Bending moment			Ptreq	0.58	%	
% minimum reinforcement			Pt min	0.18	%	
Area of reinf. Required			Ast Req (BM)	3,887	sqmm/m	
Area of reinforcement provided			Ast prv	3,897.75	sqmm/m	
Top reinforcement Along Parallel Edge						
Area of reinf. Required			Ast req	1350	sqmm/m	
Area of reinforcement provided			Ast provided	1369	sqmm/m	
			Check	OK		
Bottom reinforcement Along Perpendicular Edge						
Weight of pilecap + Overburden weight of soil		Soil Wt. + Pile-cap Wt.		469.69	kN	
Total Weight on Pile		Pcomb + Soil Wt. + Pile-cap Wt.	Ptotal	4,079.44	kN	
Forces On Piles						
Load transfer to pile P1		Ptotal/(No of Piles)-(Mux/(Dp/1000))		1,570.42	kN	
Load transfer to pile P2		Ptotal/(No of piles)+(Mux/(Dp*2/1000))-(Muy/(Ap/1000))		1,259.37	kN	
Load transfer to pile P3		Ptotal/(No of piles)+(Mux/(Dp*2/1000))+(Muy/(Ap/1000))		1,249.64	kN	
Effective depth of pilecap		Depth - cover - 20/2	Deff	690	mm	
Effective width of pile cap		Pile dia + 2 x Offset	Beff	1,050	mm	
offset from column face			DfCol	0.68	m	
Bending moment due to pile load			Bmux	1071.86	kN-m	
% reinf. Required for Bending moment			Ptreq	0.61	%	
% minimum reinforcement			Pt min	0.18	%	Clause 7.12.2.1
Area of reinf. Required			Ast Req (BM)	4,235	sqmm/m	
Area of reinforcement provided			Ast prv	4406	sqmm/m	
Top reinforcement Along Perpendicular Edge						
Area of reinf. Required			Ast req	1350	sqmm/m	
Area of reinforcement provided			Ast provided	1369	sqmm/m	
			Check	OK		
Step 9)Design for Shear						
Weight of pilecap + Overburden weight of soil		Soil Wt. + Pile-cap Wt.		469.69	kN	
Total Weight on Pile		Pcomb + Soil Wt. + Pile-cap Wt.	Ptotal	4,523.88	kN	
Forces On Piles						
Load transfer to pile P1		Ptotal/(No of Piles)-(Mux/(Dp/1000))		1,522.26	kN	

7.12.2.1 — Area of shrinkage and temperature reinforcement shall provide at least the following ratios of reinforcement area to gross concrete area, but not less than 0.0014:

(a) Slabs where Grade 280 or 350 deformed bars are used0.0020

(b) Slabs where Grade 420 deformed bars or welded wire reinforcement are used.....0.0018

(c) Slabs where reinforcement with yield stress exceeding 420 MPa measured at a yield strain of 0.35 percent is used $\frac{0.0018 \times 420}{f_y}$

Load transfer to pile P2	Ptotal/(No of piles)+(Mux/(Dp*2/1000))-(Muy/(Ap/1000))				1,505.17	kN		
Load transfer to pile P3	Ptotal/(No of piles)+(Mux/(Dp*2/1000))+(Muy/(Ap/1000))				1,496.44	kN		
Along Parallel Edge								
Section location from column center					635.00	mm		
Data For Pile								
Pile No	Load (kN)		Covered(mm)	% covered	Shear(kN)			
P1	1,522.26	1	0	0	0			
P2	1,505.17	2	72.5	9.67	1359.67			
P3	1,496.44	2	72.5	9.67	1351.78			
Design Shear Force					Vu	1359.67	kN	
Effective depth of pilecap	Depth - cover - 20- 20/2				Deff	670	mm	
Effective width of pile cap					Beff	2,098.95	mm	
Reinforcement required					pt	0.0058		
					Vu*d/Mu	0.95		
design shear strength of concrete					φVc	853.45	kN	clause 11.2.2.1
Check					Shear Reinforcement Required			
					Vs	675	kN	
					Vs perm	4150.83	kN	clause 11.4.7.9
					OK			
Shear Reinforcement Calculations								
Area of shear reinforcement required					Asv req	2398.59	sqmm/m	
Provided Shear reinforcement					Asv prv	9928	sqmm/m	
Shear capacity by Shear reinforcement					Vscap	2793.7	kN	
Check (φ * (Vc + Vs) > Vu)					Vu < φVc+Vs Capacity Hence Ok			
Along Perpendicular Edge								
Weight of pilecap + Overburden weight of soil	Soil Wt. + Pile-cap Wt.				469.69	kN		
Total Weight on Pile	Pcomb + Soil Wt. + Pile-cap Wt.				Ptotal	4,079.44	kN	
Forces On Piles								
Load transfer to pile P1	Ptotal/(No of Piles)-(Mux/(Dp/1000))				1,570.42	kN		
Load transfer to pile P2	Ptotal/(No of piles)+(Mux/(Dp*2/1000))-(Muy/(Ap/1000))				1,259.37	kN		
Load transfer to pile P3	Ptotal/(No of piles)+(Mux/(Dp*2/1000))+(Muy/(Ap/1000))				1,249.64	kN		
Section location from column center					745.0	mm		
Pile No	Load (kN)		Covered(mm)	% covered	Shear(kN)			
P1	1,570.42	2	37.47	5.00	1491.97			
P2	1,259.37	2	578.73	77.16	287.58			
P3	1,249.64	2	578.73	77.16	285.36			
Design Shear Force					Vu	1491.97	kN	
Effective depth of pilecap	Depth - cover - 20/2				Deff	690	mm	
Effective width of pile cap					Beff	1,602.18	mm	
Reinforcement required					pt	0.0061		
					Vu*d/Mu	0.96		
					φVc	676.366187	kN	clause 11.2.2.1
					Shear Reinforcement Required			
					Vs	1,087	kN	
					Vs perm	3263.02	kN	clause 11.4.7.9
					OK			
Shear Reinforcement Calculations								
Area of shear reinforcement required					Asv req	3752.48	Sqmm	
Provided Shear reinforcement					Asv prv	15128.115	Sqmm	
Shear capacity by Shear reinforcement					Vscap	4384.12773	kN	
Check (φ * (Vc + Vs) > Vu)					Vu < φVc+Vs Capacity Hence Ok			

11.2.2.1 — For members subject to shear and flexure only,

$$V_c = \left(0.16\lambda\sqrt{f'_c} + 17\rho_w \frac{V_u d}{M_u} \right) b_w d \quad (11-5)$$

but not greater than $0.29\lambda\sqrt{f'_c} b_w d$. When computing V_c by Eq. (11-5), $V_u d / M_u$ shall not be taken greater than 1.0, where M_u occurs simultaneously with V_u at section considered.

11.4.7.9 $0.66\sqrt{f'_c} b_w d$

11.2.2.1 — For members subject to shear and flexure only,

$$V_c = \left(0.16\lambda\sqrt{f'_c} + 17\rho_w \frac{V_u d}{M_u} \right) b_w d \quad (11-5)$$

but not greater than $0.29\lambda\sqrt{f'_c} b_w d$. When computing V_c by Eq. (11-5), $V_u d / M_u$ shall not be taken greater than 1.0, where M_u occurs simultaneously with V_u at section considered.

11.4.7.9 $0.66\sqrt{f'_c} b_w d$

Step 10) Design of Face reinforcement																				
Area of side face reinf. Required			Asfr Req	187.5	Sqmm															
Area of side face reinf. Provided			Asfr pro	213	Sqmm															
Step 11) Design For Column Load Transfer																				
Maximu Axial load on column		Axial Load	P	4,054.19	kN															
Area of column		Bc x Dc	A2	0.48	sqm	Clause 10.14														
Area of pilecap base		Area of Pilecap	A1	5.43	sqm	Clause 10.14														
Pilecap Base area		Base Area		5.43	sqm															
Modification Factor		Modification Factor		SquareRoot(A1/A2) <= 2																
		SquareRoot(A1/A2)		3.36																
		Thus, Modification Factor		2		Clause 10.14														
$\Phi_1 P_{nb}$		$\Phi_1 \times 0.85 \times \text{Modification Factor} \times A_2 \times F_{ck} \times 1000$																		
		$0.65 \times 0.85 \times 0.48 \times 20 \times 1000$																		
Concrete Bearing capacity			$\Phi_1 P_{nb}$	10608	kN	Clause 10.14														
Check				Hence Safe																
Area Of Dowels					- sqmm															

10.14 — Bearing strength

10.14.1 — Design bearing strength of concrete shall not exceed $\phi(0.85f'_c A_1)$, except when the supporting surface is wider on all sides than the loaded area, then the design bearing strength of the loaded area shall be permitted to be multiplied by $\sqrt{A_2/A_1}$ but by not more than 2.