

26 A (Slenderness)	=	Constant
27 $A_c$	=	Cross Sectional Area of Concrete in $\text{mm}^2$
28 $A_{ceff}$	=	Effective Cross Sectional Area of Concrete used for shear in $\text{mm}^2$
29 Ash	=	Volume of confining hoops in $\text{mm}^3$
30 $A_{s\ est}$	=	Estimated area of longitudinal reinforcement for slenderness check in $\text{mm}^2$
31 $A_{sw}/s$	=	Area of Shear reinforcement required in $\text{sqmm}/\text{m}$
32 $A_{swmax}/s$	=	Maximum Area of Shear Reinforcement in $\text{sqmm}/\text{m}$
33 b	=	Effective Width of Column in mm
34 $b_j$	=	Effective joint width along Column direction considered in mm
35 B (General Data)	=	Width / Smaller Dimension of Column in mm
36 B (Slenderness)	=	Constant
37 $b_{wo}$	=	Thickness of web of a wall in mm
38 C (Slenderness)	=	Constant
39 c	=	Factor depending on the curvature distribution
40 D	=	Depth / Larger Dimension of Column OR Diameter of Circular Column in mm
41 d	=	Effective Depth of Column in mm
42 $D_k$	=	Diameter Of core measured to the outside of circular link in mm
43 $E_c$	=	Modulus of elasticity of concrete in $\text{N}/\text{sqmm}$
44 $E_s$	=	Modulus of elasticity of Reinforcement in $\text{N}/\text{sqmm}$
45 e2	=	Deflection to calculate second order moment in mm
46 e0	=	Minimum eccentricity in mm
47 $f_{ck}$	=	Characteristic Cylindrical strength of Concrete $\text{N}/\text{sqmm}$
48 $f_{cPerm}$	=	Permissible Stress in Concrete required in $\text{N}/\text{sqmm}$
49 $f_{ctm}$	=	Mean value of axial tensile strength of Concrete in $\text{N}/\text{sqmm}$
50 $f_{st}$	=	Stress in Reinforcement in $\text{N}/\text{sqmm}$
51 $f_{stPerm}$	=	Permissible Stress in Reinforcement required in $\text{N}/\text{sqmm}$
52 $f_{yd}$	=	Design value of Reinforcement yield strength in $\text{N}/\text{sqmm}$
53 $f_{yd, h}$	=	Design value Of yield strength Of the horizontal web reinforcement in $\text{N}/\text{sqmm}$
54 $f_{ctd}$	=	Tensile Strength of Concrete in $\text{N}/\text{sqmm}$
55 $f_{ywd}$	=	Design yield stress for shear reinforcement in $\text{N}/\text{sqmm}$
56 hcr	=	Height Of critical region above base Or basement story in m
57 $h_{jc}$	=	Distance between extreme layer of column reinforcement along Column direction considered in mm

58	$h_{jw}$	=	Distance between top and bottom reinforcement of Beam along Column direction considered in mm
59	$i$	=	Radius of Gyration of uncracked section in mm
60	$K_1$	=	Crack width co-efficient For high bond bars (value = 0.8)
61	$K_2$	=	Crack width co-efficient For bending (value = 0.5)
62	$K_3$	=	Crack width constant (value = 3.4)
63	$K_4$	=	Crack width constant (value = 0.5)
64	$K_r$	=	Correction factor depending On the axial load
65	$k_w$	=	Factor reflecting the prevailing failure mode In structural systems With walls
66	$l_o$	=	Effective length Of column in mm
67	$l_w$	=	Length Of cross-section Of wall in mm
68	$M_{ed}$	=	Design bending moment from the analysis For the seismic design situation in kN-m
69	$m_{geoD}$	=	Moment due To geometric imperfections along D in kN-m
70	$m_{geoB}$	=	Moment due To geometric imperfections along B in kN-m
71	$M_{ux}$	=	Factored moment Along D (Moment About Major Axis) in kN-m
72	$M_{uy}$	=	Factored moment Along B (Moment About Minor Axis) in kN-m
73	$M_{Cap}$	=	Moment capacity Of section For NA angle at design $P_u$ in kN
74	$M_{Res}$	=	Resultant design moment at angle To local major axis in kN-m
75	$M_{2B}$	=	Additional moment due To slenderness about minor axis (Along B) in kN-m
76	$M_{2D}$	=	Additional moment due To slenderness about major axis (Along D) in kN-m
77	$M_2$	=	Nominal second order moment in kN-m
78	$M_{01}$	=	First order End moments in kN-m
79	$M_{02}$	=	First order End moments in kN-m
80	$n$	=	Relative axial force in kN
81	$n_{bal}$	=	Value Of $n$ at maximum moment Of resistance in kN
82	$N_{ed}$	=	Design axial force from the analysis For the seismic design situation in kN
83	$q$	=	Behavior factor
84	$q_o$	=	Basic value Of the behavior factor
85	$r_m$	=	Moment Ratio, $M_{01} / M_{02}$
86	$s_{l,max}$	=	Maximum Longitudinal Spacing of stirrups in mm
87	$T_1$	=	Fundamental period Of the building In the horizontal direction Of interest in sec
88	$T_c$	=	Corner period at the upper limit Of the constant acceleration region Of the elastic Spectrum in sec

89	$V_{Rd,max}$	=	Maximum Shear resistance of Section in kN
90	$V_d$	=	Normalized axial force in column above joint in kN
91	$V_{Ed,x}$	=	Design shear force at the ULS Long B in kN
92	$V_{Ed,y}$	=	Design shear force at the ULS Long D in kN
93	$v'_{ed}$	=	Shear force in a wall from the analysis for the seismic design situation in kN
94	$V_{ur}$	=	Factored resultant shear force acting on the column in kN
95	$V_{jhd}$	=	Compressive strength of Concrete in the presence of transverse tensile strain in kN
96	$W_{cr}$	=	Surface Crack Width in mm
97	$W_{cr,Perm}$	=	Permissible Crack Width required in mm
98	$X_u$	=	Neural axis Depth in mm
99	$z$	=	Internal lever arm in mm

**Code References:****EN 1992 - 1 - 1 - 2004 Base**

	ELEMENT		CLAUSE / table
1	Max area of reinforcement	:	Cl. 9.5.2 (3)
2	Min area of reinforcement	:	Cl. 9.5.2 (2)
3	Minimum Eccentricity Calc	:	6.1 (4)
4	Slenderness Moments	:	5.8.8.2
5	Design of horizontal links	:	6.2.3
6	Determine shear capacity without shear reinforcement	:	6.2.2
7	Crack width calculation	:	7.3.4

**BS EN 1998-1:2004 (E)**

	ELEMENT		CLAUSE / table
1	Spacing of special confining reinforcement	:	Cl.5.4.3.2.2 (8)
2	C/s area of special confining reinforcement	:	Cl.5.2.3.4 (3)
3	Shear resistance of ductile wall	:	Cl.5.5.2.4.1
4	Ductile wall (Bending and Shear)	:	Cl.5.4.3.4
5	Special provisions for ductile walls	:	Cl.5.4.2.4 and Cl.5.4.2.5
6	Design for DCM	:	Cl.5.4
7	Design for DCH	:	Cl.5.5

**General Data**

Column No.	:	C1
Level	:	0 m To 5.25 m

Design Code	=	EN 1992 - 1 - 1 - 2004 Base	
Type of Frame	=	Non Ductile	
Grade Of Concrete ( $f_{ck}$ ) (Cylindrical)	=	C25/30	N/sqmm
Partial Factor for concrete, $\gamma_c$ (Persistent and Transient)	=	1.5	
Partial Factor for concrete, $\gamma_{c acc}$ (Accidental)	=	1.2	
Grade Of Steel ( $f_{yk}$ )	=	Fy500	N/sqmm
Partial Factor for reinforcing steel, $\gamma_s$ (Persistent and Transient)	=	1.15	
Partial Factor for reinforcing steel, $\gamma_{s acc}$ (Accidental)	=	1	
Column B	=	300	mm
Column D	=	300	mm
$A_c$	=	90000	sqmm
Clear Cover	=	35	mm
Clear Floor Height @ B,loB	=	5250	mm
Clear Floor Height @ D,loD	=	5250	mm
No Of Floors	=	1	
No Of Columns In Group	=	1	
Column Type Along D	=	UnBraced	
Column Type Along B	=	UnBraced	
Minimum eccentricity check	=	Simultaneously (Both Axis)	
Effective Length Along D	=	1.2	
Effective Length Along B	=	1.2	

**Load Data**

Analysis Reference No.	=	1	
Critical Analysis Load Combination	:	2	
Load Combination	=	[1] : (LOAD 1: LOAD CASE 1)	
Critical Location	=	Mid Joint	
Ned(top joint)	=	420.17	kN
Mux(top joint)	=	0	kNm
Muy(top joint)	=	0	kNm
Vux(top joint)	=	0	kN
Vuy(top joint)	=	0	kN
Ned(bottom joint)	=	420.17	kN
Mux (bottom joint)	=	0	kNm
Muy (bottom joint)	=	0	kNm
Vux (bottom joint)	=	0	kN
Vuy(bottom joint)	=	0	kN

**Minimum Eccentricity,**

Since Axial Force is compressive, Min. Eccentricity check to be performed

**Check, e0**

$$\begin{aligned}
 \text{Minimum Eccentricity Along D:} &= D / 30 \\
 \text{Minecc (e0D)} &= 10 \quad \text{mm} \\
 &= 20 \quad \text{MM, Since } < 20 \\
 \text{Mmind} &= \text{Ned} \times \text{Minimum Eccentricity} \\
 &= 8.4 \quad \text{kNm}
 \end{aligned}$$

$$\begin{aligned}
 \text{Minimum Eccentricity Along B:} &= B / 30 \\
 \text{Minecc (e0B)} &= 10 \quad \text{mm} \\
 &= 20 \quad \text{MM, Since } < 20 \\
 \text{Mminb} &= \text{Ned} \times \text{Minimum Eccentricity} \\
 &= 8.4 \quad \text{kNm}
 \end{aligned}$$

**Geometric imperfection, ei**

$$\begin{aligned}
 \theta_0 &= 0.005 \\
 \alpha_n &= 0.873 \\
 \alpha_m &= 1 \\
 \theta_1 &= 0.00436 \quad \text{Radian}
 \end{aligned}$$

$$\begin{aligned}
 \text{Eccentricity , (ei) (along both the directions)} &= 13.75 \quad \text{mm} \\
 \text{MgeoD} &= 5.78 \quad \text{kNm} \\
 \text{MgeoB} &= 5.78 \quad \text{kNm}
 \end{aligned}$$

**Slenderness Check**

$$\begin{aligned}
 A_{st \text{ Prv}} &= 2060.88 \quad \text{sqmm} \\
 \omega &= A_{st \text{ prv}} \times f_{yd} / (B \times D \times f_{cd}) \\
 &= 0.7
 \end{aligned}$$

**Calculation of SLENDERNESS CHECK**

	Along D	Along B
Critical Load Combination	[1] : (LOAD 1: LOAD CASE 1)	[1] : (LOAD 1: LOAD CASE 1)
Ned (kN)	420.17	420.17
Mo1 (kNm)	0	0
Mo2 (kNm)	0	0
Radius of Gyration (i) (mm)	86.71	86.71
$\Phi_{ef}$	2.14	2.14
$\Lambda = 1 / (1 + 0.2 \times \Phi_{ef})$	0.7	0.7

$B = \text{Sqrt}(1 + 2 \omega)$	1.55	1.55
$r_m = M_{o1} / M_{o2}$	0	0
$C = 1.7 - r_m$	1.7	1.7
$n = N_{ed} / (B \times D \times f_{cd})$	0.3295	0.3295
Slenderness ratio ( $\lambda$ ) = $l_o / i$	72.66	72.66
Permissible Limits ( $\lambda_{lim}$ ) = $A \times B \times C / \text{sqrt}(n)$	64.26	64.26
	Hence, Column is Slender	Hence, Column is Slender

### Calculation of Slenderness Moment

	Along D	Along B
$\nu = 1 + \omega$	1.7	1.7
$n_{bal}$	0.4	0.4
$K_r = \text{Min}((\nu - n) / (\nu - n_{bal}), 1)$	1	1
$c$ (Constant)	10	10
$I_s$ (mm)	86.71	86.71
$d_{eff}$ , slenderness = $(D' / 2) + I_s$ (mm)	134.08	134.08
$\beta = 0.35 + f_{ck} / 200 - \lambda / 150$	-0.009	-0.009
$1 / r_o = f_{yd} / E_s \times (0.45 \times d_{eff}, \text{slenderness}) \times 10^{-5}$	3.6	3.6
$K \phi = \text{Max}((1 + \beta \times \Phi_{ef}), 1)$	1	1
$1 / r = K_r \times K \phi \times (1 / r_o) \times 10^{-5}$	3.6	3.6
$e_2 = (1 / r) \times (l_o^2 / c)$ (mm)	143	143
$M_{oe} = 0.4 \times \text{Min}(\text{top, bottom}) + 0.6 \times \text{Max}(\text{top, bottom})$ (kNm)	3.36	3.36
$M_2 = e_2 \times N_{ed}$ (kNm)	60.08	60.08
Mid Moment = $M_{oe} + M_2$ (kNm)	63.45	63.45

### Note:

$d_{eff}$ ,  
slenderness = Effective Depth of the section along the direction considered.

$D'$  = Depth of the section along the direction considered.

### Calculation of Design Moment

Direction	Manalysis	Mmin	Mgeo	Mdesign	M2	Mdesign-final
	A	B	C	D	E	F
Major Axis - Mux (top)	0	8.4	5.78	8.4	60.08	38.45
Major Axis Mux (bottom)	0	8.4	5.78	8.4	60.08	38.45
Major Axis Mux (mid)	---	---	---	---	---	63.45
Minor Axis Muy (top)	0	8.4	5.78	8.4	60.08	38.45
Minor Axis Muy (bottom)	0	8.4	5.78	8.4	60.08	38.45
Minor Axis Muy (mid)	---	---	---	---	---	63.45

Where

A	= Moments directly from analysis
B	= Moments due to minimum eccentricity
C	= Moments due to geometrical imperfection
D	= Max of (M <sub>analysis</sub> +M <sub>Geo</sub> ) , M <sub>min</sub>
E	= Moment due to slenderness effect
F	= M <sub>design</sub> + M <sub>2</sub> / 2
Top.Bottom	
F Mid	= M <sub>oe</sub> +M <sub>2</sub>

**Final Critical Design Forces**

Critical Case - Axial Load &amp; BiAxial Bending

P <sub>u</sub>	=	420.17	kN
M <sub>ux</sub>	=	63.45	kNm
M <sub>uy</sub>	=	63.45	kNm

**Resultant Moment (Combined Action)****Moment Capacity Check**

P <sub>t</sub> Calculated	=	2.29	
Reinforcement Provided	=	4-T20 + 4-T16	
Load Angle	=	Tan <sup>-1</sup> (M <sub>uy</sub> /M <sub>ux</sub> )	
	=	45	deg
M <sub>Res</sub>	=	89.73	kNm
M <sub>Cap</sub>	=	95.4	kNm
Capacity Ratio	=	M <sub>Res</sub> / M <sub>Cap</sub>	
	=	0.94 < 1	

**Biaxial Bending Check**

λ <sub>D</sub> /λ <sub>B</sub>	=	1	
λ <sub>B</sub> /λ <sub>D</sub>	=	1	
e <sub>D</sub> (top)	=	91.501	mm
e <sub>D</sub> (bot)	=	91.501	mm
e <sub>B</sub> (top)	=	91.501	mm
e <sub>B</sub> (bot)	=	91.501	mm
(e <sub>D</sub> top/D)/(e <sub>B</sub> top/B)	=	1	mm
(e <sub>B</sub> top/B)/(e <sub>D</sub> top/D)	=	1	mm
(e <sub>D</sub> bot/D)/(e <sub>B</sub> bot/B)	=	1	mm
(e <sub>B</sub> bot/B)/(e <sub>D</sub> bot/D)	=	1	mm

Check for Bi-axial bending Consider Biaxial

**Check For Minimum Vertical Reinforcement**

Minimum p <sub>t</sub> -1(User Defined)	=	0.2	%
---	---	-----	---

As,min-1(as per user defined pt-1)	=	Minimum pt-1 x Ac / 100	
	=	180	sqmm
Load Combination	=	[1] : (LOAD 1: LOAD CASE 1)	
Ned	=	420.17	kN
fyd	=	434.78	N/sqmm
Minimum pt-2 (as per Ned)	=	0.1 x Ned / ( fyd x Ac)	
	=	0.1074	%
As,min-2 (as per Ned)	=	Minimum pt-2 x Ac / 100	
	=	96.64	sqmm
As,min	=	Max (As,min-1 , As,min-2)	
	=	180	sqmm
As provided	=	2060.88	sqmm
As provided	>	As,min Hence, OK	

**Design Of Shear****Along D**

Critical Analysis Load Combination	:	2	
Critical Load Combination	=	[1] : (LOAD 1: LOAD CASE 1)	
Design shear force, V <sub>uy</sub>	=	0	kN
N <sub>Ed</sub>	=	420.17	kN
Design shear stress ,V <sub>Ed</sub>	=	0	N/mm <sup>2</sup>
Calculation for Concrete Strut Capacity V <sub>Rdmax</sub>			
lever arm, z	=	255	mm
v <sub>1</sub>	=	0.54	
V <sub>Rd,max</sub> cot θ = 2.5	=	2.37	N/mm <sup>2</sup>
V <sub>Rd,max</sub> cot θ = 1	=	3.44	N/mm <sup>2</sup>
V <sub>Rd,max</sub>	=	181.61	kN
Check		V <sub>Rd,max</sub> > V <sub>uy</sub> Hence, OK	
VRD,c	=	88.41	kN
As tension(50%)	=	1030.44	sqmm
CRdc	=	0.18/γ <sub>c</sub>	
	=	0.12	
A <sub>ceff</sub>	=	76500	sqmm
d <sub>eff</sub>	=	255	mm
k	=	MIN(1 + SQRT(200 / d <sub>eff</sub> ),2)	
	=	1.8856	
ρ <sub>1</sub>	=	As <sub>main</sub> / A <sub>ceff</sub>	
	=	0.0135	%
k <sub>1</sub>		0.15	



$$\sigma_{cp} = \frac{N_{Ed}}{B \times D} = 2.8333 \text{ N/mm}^2$$

Shear check No Shear Reinforcement Required  
Since  $VRD,C > V_{uy}$

### Along B

Critical Analysis Load Combination : 2

Critical Load Combination = [1] : (LOAD 1: LOAD CASE 1)

Design shear force,  $V_{ux}$  = 0 kN

$N_{Ed}$  = 420.17 kN

Design shear stress,  $v_{Ed}$  = 0  $\text{N/mm}^2$

Calculation for Concrete Strut Capacity  $V_{Rd,max}$

lever arm,  $z$  = 255 mm

$v_1$  = 0.54

$V_{Rd,max} \cot \theta = 2.5$  = 2.37  $\text{N/mm}^2$

$V_{Rd,max} \cot \theta = 1$  = 3.44  $\text{N/mm}^2$

$V_{Rd,max}$  = 181.61 kN

Check  $V_{Rd,max} > V_{ux}$  Hence, OK

$VRD,c$  = 88.41 kN

As tension(50%) = 1030.44 sqmm

$CR_{dc}$  = 0.18 /  $\gamma_c$

= 0.12

$A_{ceff}$  = 76500 sqmm

$b_{eff}$  = 255 mm

$k$  =  $\text{MIN}((1 + \text{SQRT}(200 / b_{eff})), 2)$

= 1.8856

$\rho_1$  =  $A_{s\text{main}} / A_{ceff}$

= 0.0135 %

$k_1$  = 0.15

$\sigma_{cp}$  =  $\frac{N_{Ed}}{B \times D} = 2.8333 \text{ N/mm}^2$

Shear check No Shear Reinforcement Required  
Since  $VRD,C > V_{ux}$

### Design Of Links

Length of End Zone:

Maximum dimension of column = 300 mm

Links in the zone where special confining links are not required or End Zone

Normal Links

Diameter of link Provided	=	8	mm
Check for minimum diameter of link			
Main Reinforcement (Bundled / Single)	=	Single	
Number of Rebars in Bundled	=	1	
Maximum diameter of Vertical Reinforcement	=	20	mm
Effective diameter of Vertical Reinforcement	=	20	mm
Minimum dia-1 (6mm)	=	6	mm
Minimum dia-2	=	Effective diameter / 4	
	=	5	mm
Minimum dia	=	Max (Minimum dia-1, Minimum dia-2)	
	=	6	mm
Diameter of link Provided	>	Minimum dia	Hence, OK
Criterion for spacing of normal links			
Min. Longitudinal Bar dia X 20	=	320	mm
Min. dimension of column	=	300	mm
Max. Permissible	=	400	mm
Max. Permissible (User Input)	=	300	mm
Provided spacing	=	300	mm

Links at End Zone

Criterion for spacing of End Zone links

0.6 x Min. Longitudinal Bar dia X 20	=	192	mm
0.6 x Min. dimension of column	=	180	mm
0.6 x Max. Permissible	=	240	mm
Max. Permissible (User Input)	=	300	mm
Provided spacing	=	175	mm

**Table For Links**

	Required			Provided	
	Normal Design	Shear Design	Ductile/End Zone	Normal Zone	Ductile/End Zone
Link Dia.	8	---	8	8	8
Spacing	300	---	175	300	175